Shenzhen Belling Efficiency Testing Lab Co., Ltd

Report No.: BL220426009-9

## Test report of

| Date of issue | $2022-05-31$ |
| :--- | :--- |
| Version | 1.0 |
| Total pages | 20 |

IES LM-79-08

## Approved Method: Electrical and Photometric

## Measurements of Solid-State Lighting Products

## Applicant:

P.Q.L., Inc.

## Address:

2285 Ward Avenue
Simi Valley, CA 93065

## For Product:

High Bay Luminaires (Commercial and Industrial)

Model No.:
CHB3-100-D-MV-30K-170S, CHB3-100-D-MV-65K-170S

Test laboratory: Shenzhen Belling Efficiency Testing Lab Co., Ltd, 1Floor, No. 1 Building, Meibaohe Industrial Park, Dalang Street, Longhua District, Shenzhen, Guangdong Prov. 518101 China.


Note: The test data was only valid for the test sample(s). This test report is prepared for the customer shown above and for the device described herein. It may not be duplicated or use in part without prior written consent from Shenzhen Belling Efficiency Testing Lab Co., Ltd. This report must not be used by the customer to claim product certification, approval, or endorsement By NVLAP, NIST, or any agency of the U.S. Government.

## 1 General

### 1.1 Product Information

| Manufacturer | P.Q.L., Inc. |
| :--- | :--- |
| Manufacturer Address | 2285 Ward Avenue <br> Simi Valley, CA 93065 |
| Brand Name | PQL |
| Luminaire Type | High Bay Luminaires (Commercial and Industrial) |
| Model Number | CHB3-100-D-MV-30K-170S, <br> CHB3-100-D-MV-65K-170S |
| Rated Inputs | AC 100-277V, 50/60Hz |
| Rated Power | 100 W |
| Nominal CCT | $3000 \mathrm{~K}, 6500 \mathrm{~K}$ |
| Dimming Capability | Continuous, 0-10V |
| Integral Control Sensors | No |
| Date of Receipt Samples | $2022-04-26$ |
| Date of test | $2022-04-27$ to 2022-05-24 |
| Burning Time Before Test | 0 hour(For New Products) |

### 1.2 Standards or methods

- ANSI C78.377-2017:Specifications for the Chromaticity of Solid State Lighting Products
- ANSI C82.77-10:2014:Harmonic Emission Limits - Related Power Quality Requirements for Lighting Equipment - Solid State
- CIE Publication No.13.3-1995:Method of Measuring and Specifying Color Rendering of Light Sources
- IESNA LM-79-08 Approved Method: Electric \& Photometric Measurement of Solid-state Lighting Products


### 1.3 Equipment list

| Device | Manufacture | Model No. | Serial No. | Calibration <br> due date |
| :---: | :---: | :---: | :---: | :---: |
| Goniophotometeric System | SENSING | GMS-3000 | N.A | $2023-04-08$ |
| AC Power Source | ALL POWER | APW-105N | 970780 | $2023-04-10$ |
| Total Luminous Flux Standard <br> Lamp | SENSING | $110 \mathrm{~V} / 100 \mathrm{~W}$ | S13100188 | $2023-03-30$ |
| Total Luminous Flux Standard <br> Lamp | OSRAM | $12 \mathrm{~V} / 20 \mathrm{~W}$ | LSD1220173 | $2023-03-30$ |
| Digital Power Meter | YOKOGAWA | WT310 | C2QM02030V | $2023-04-10$ |
| Thermostatic stabilized <br> photometric sphere | SENSING | SPR-600M | N.A | $2023-04-08$ |
| Digital Power Meter | YOKOGAWA | WT210 | 91L929742 | $2023-04-10$ |
| Spectral radiometer | SENSING | SPR-3000 | S1101108 | $2023-04-08$ |
| Environment Measurer | XUYAO | HS-1 | N/A | $2023-03-30$ |
| Environment Measurer | XUYAO | HSS-1 | N/A | $2023-03-30$ |
| Stop watch | KISLO | K610 | N/A | $2023-04-14$ |
| TECMAN | TD8901 | 026141 | $2022-09-08$ |  |

Statement of Traceability: Shenzhen Belling Efficiency Testing Lab Co., Ltd attests that all calibration has been performed using suitable standards traceable to national primary standards and International System of Unit (SI).

## 2 Test conducted and method

### 2.1 Ambient Condition

The ambient temperature in which measurements are being taken was maintained at $25^{\circ} \mathrm{C} \pm 1^{\circ} \mathrm{C}$, the air flow around the sample(s) being tested did not affect the performance.

### 2.2 Power Supply Characteristics

The AC power supply had a sinusoidal voltage wave shape at the prescribed frequency $(60 \mathrm{~Hz})$ such that the RMS summation of the harmonic components does not exceed 3 percent of the fundamental during operation of the test item.

The voltage of AC power supply (RMS voltage) applied to the device under test was regulated to within $\pm 0.2$ percent under load.

### 2.3 Seasoning and Stabilization

No seasoning was performed in accordance with IESNA LM-79-08. And before the measurement, the sample was stabilized until the light output and power variations were less than $0.5 \%$ in 30 minutes intervals ( 3 readings, 15 minutes apart).

### 2.4 Integrating Sphere System

The system includes AC power source, digital power meter, DC power supply, spectrophotometer, and integrating sphere. The integrating sphere system is calibrated by standard light source before measurement. The system and standard light source has been calibrated regularly and traceable to the National Primary Standards. $4 \pi$ geometry was used during measurement. The product was operated in its intended orientation in application and was recorded in this report.

Integrating Sphere Uncertainty: The uncertainty of the light output (luminous flux) measurements is $\mathrm{U}=1.8 \%(\mathrm{~K}=2)$, at the $95 \%$ confidence level. The uncertainty of the correlated color temperature measurements is $\mathrm{U}=20 \mathrm{~K}(\mathrm{~K}=2)$, at the $95 \%$ confidence level. The uncertainty of the CRI is $\mathrm{U}=1.8(\mathrm{~K}=2)$, at the $95 \%$ confidence level. The uncertainty of power meter AC current $\mathrm{U}=0.18 \%$ of rdg, AC Voltage $\mathrm{U}=0.16 \%$ of rdg, Power $\mathrm{U}=0.20 \%(\mathrm{~K}=2)$, at the $95 \%$ confidence level.

### 2.5 Goniophotometer System

The goniophotometer system is calibrated by standard light source before measurement. The standard light source has been calibrated regularly and traceable to the National Primary Standards.

Type C goniophotometer was used for measuring total luminous flux, luminous intensity distribution, and color spatial uniformity. The product was operated in its intended orientation in application and was recorded in this report. The method according to IESNA LM-79-08 following chapter.

Goniophotometer Uncertainty : The uncertainty of the luminous intensity is $\mathrm{U}=1.6 \%(\mathrm{~K}=2)$, at the $95 \%$ confidence level.

## 3 Test Result Summary

3.1 Integrating Sphere System (Total operating time for integrating sphere test: 1.0 hour)
3.1.1 Model Number: CHB3-100-D-MV-30K-170S

Electrical data

| Input Voltage(V) | Frequency (Hz) | Input Current (A) | Power (W) | Power Factor |
| :---: | :---: | :---: | :---: | :---: |
| 120.03 | 60 | 0.835 | 99.78 | 0.995 |

Photometric data

| Luminous Flux (Im) | Efficacy ( $1 \mathrm{~m} / \mathrm{W}$ ) | CCT (K) |
| :---: | :---: | :---: |
| 15685.24 | 157.2 | 2900 |

## Chromaticity Coordinate

| Duv | $x$ | $y$ | $u^{\prime}$ | $v^{\prime}$ |
| :---: | :---: | :---: | :---: | :---: |
| -0.00038 | 0.4437 | 0.4053 | 0.2544 | 0.5229 |

Color Rendering

| CRI | R9 | Rf | Rg | Rcs,h1(\%) |
| :---: | :---: | :---: | :---: | :---: |
| 73.2 | -16 | 75 | 96 | -14 |

## Spectral Distribution




## $7 / 4$ Step Quadrangle



## ANSI/IES TM-30-18 Color Rendition Report



Jolors are for visual orientation purposes only. Created with the ANSI/IES TH-30-18 Calculator Version 2.00.

### 3.1.2 Model Number: CHB3-100-D-MV-65K-170S

Electrical data

| Input Voltage(V) | Frequency (Hz) | Input Current (A) | Power (W) | Power Factor |
| :---: | :---: | :---: | :---: | :---: |
| 120.01 | 60 | 0.836 | 100.01 | 0.997 |

## Photometric data

| Luminous Flux (Im) | Efficacy ( $1 \mathrm{~m} / \mathrm{W}$ ) | CCT (K) |
| :---: | :---: | :---: |
| 17331.54 | 173.3 | 6366 |

Chromaticity Coordinate

| Duv | $x$ | $y$ | $u^{\prime}$ | $v^{\prime}$ |
| :---: | :---: | :---: | :---: | :---: |
| +0.00624 | 0.3144 | 0.3367 | 0.1962 | 0.4726 |

Color Rendering

| CRI | R9 | Rf | Rg | Rcs,h1(\%) |
| :---: | :---: | :---: | :---: | :---: |
| 71.4 | -32 | 73 | 92 | -18 |

## Spectral Distribution



## 7/4 Step Quadrangle



## ANSI/IES TM-30-18 Color Rendition Report

| Source: | BL220426009-9 |
| :--- | :--- |
| Date: | $2022-05-31$ |

Manufacturer: P.Q.L., Inc.
Model: CHB3-100-D-MV-65K-170S







Notes: This is a recommended method for displaying ANSI/IES TM-30-18 information.

| $x$ | $\mathbf{0 . 3 1 4 4}$ | CIE | 13.3-1995 <br> $y$ |
| :---: | :---: | :---: | :---: |
| $y^{\prime}$ | $\mathbf{0 . 3 3 6 7}$ |  | (CRI) |
| $u^{\prime}$ | $\mathbf{0 . 1 9 6 2}$ | $R_{\mathrm{a}}$ | 71 |
| $v^{\prime}$ | $\mathbf{0 . 4 7 2 6}$ | $R_{9}$ | -32 |

[^0]3.2 Goniophotometer System (Total operating time for luminous intensity distribution: 1.0 hour)

### 3.2.1 Model Number: CHB3-100-D-MV-30K-170S

## Electrical data

| Input Voltage(V) | Frequency (Hz) | Input Current (A) | Power (W) | Power Factor |
| :---: | :---: | :---: | :---: | :---: |
| 120.08 | 60 | 0.831 | 99.45 | 0.9961 |

## Photometric data

| Luminous Flux (lm) | Efficacy ( $1 \mathrm{~m} / \mathrm{W}$ ) | Zonal Lumen in <br> $20-50^{\circ}(\% \mathrm{~m})$ |
| :---: | :---: | :---: |
| 15672.96 | 157.60 | 52.92 |

## Zonal Flux Diagram

## Zonal flux distribution table

| $\gamma\left({ }^{\circ}\right)$ | Average I(cd) | Zonal F(lm) | Sum F(lm) | Eff Flux(\%) | Eff Sum(\%) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 0.0 | 5891.651 | 0.000 | 0 | 0.00\% | 0.00\% |
| 5.0 | 5857.211 | 140.454 | 140.454 | 0.00\% | 0.90\% |
| 10.0 | 5766.391 | 415.813 | 556.267 | 0.00\% | 3.55\% |
| 15.0 | 5615.389 | 675.160 | 1231.427 | 0.00\% | 7.86\% |
| 20.0 | 5433.886 | 910.615 | 2142.042 | 0.00\% | 13.67\% |
| 25.0 | 5214.394 | 1116.808 | 3258.85 | 0.00\% | 20.79\% |
| 30.0 | 4951.740 | 1286.533 | 4545.383 | 0.00\% | 29.00\% |
| 35.0 | 4639.795 | 1412.421 | 5957.804 | 0.00\% | 38.01\% |
| 40.0 | 4288.636 | 1489.641 | 7447.445 | 0.00\% | 47.52\% |
| 45.0 | 3881.583 | 1512.782 | 8960.227 | 0.00\% | 57.17\% |
| 50.0 | 3426.846 | 1476.775 | 10437.002 | 0.00\% | 66.59\% |
| 55.0 | 2942.426 | 1384.892 | 11821.893 | 0.00\% | 75.43\% |
| 60.0 | 2411.711 | 1237.594 | 13059.487 | 0.00\% | 83.32\% |
| 65.0 | 1808.259 | 1025.883 | 14085.37 | 0.00\% | 89.87\% |
| 70.0 | 1200.995 | 761.962 | 14847.332 | 0.00\% | 94.73\% |
| 75.0 | 665.106 | 487.769 | 15335.101 | 0.00\% | 97.84\% |
| 80.0 | 245.566 | 243.670 | 15578.771 | 0.00\% | 99.40\% |
| 85.0 | 7.761 | 68.835 | 15647.606 | 0.00\% | 99.84\% |
| 90.0 | 1.307 | 2.483 | 15650.089 | 0.00\% | 99.85\% |
| 95.0 | 1.144 | 0.671 | 15650.76 | 0.00\% | 99.86\% |
| 100.0 | 1.144 | 0.621 | 15651.382 | 0.00\% | 99.86\% |
| 105.0 | 1.525 | 0.714 | 15652.096 | 0.00\% | 99.87\% |
| 110.0 | 1.893 | 0.893 | 15652.989 | 0.00\% | 99.87\% |
| 115.0 | 2.600 | 1.138 | 15654.127 | 0.00\% | 99.88\% |
| 120.0 | 3.241 | 1.420 | 15655.547 | 0.00\% | 99.89\% |
| 125.0 | 4.017 | 1.678 | 15657.224 | 0.00\% | 99.90\% |
| 130.0 | 4.684 | 1.892 | 15659.116 | 0.00\% | 99.91\% |
| 135.0 | 5.324 | 2.022 | 15661.138 | 0.00\% | 99.92\% |
| 140.0 | 5.800 | 2.060 | 15663.198 | 0.00\% | 99.94\% |
| 145.0 | 6.223 | 2.006 | 15665.204 | 0.00\% | 99.95\% |
| 150.0 | 6.658 | 1.897 | 15667.101 | 0.00\% | 99.96\% |
| 155.0 | 6.958 | 1.723 | 15668.824 | 0.00\% | 99.97\% |
| 160.0 | 7.053 | 1.469 | 15670.293 | 0.00\% | 99.98\% |
| 165.0 | 6.998 | 1.158 | 15671.451 | 0.00\% | 99.99\% |
| 170.0 | 6.971 | 0.829 | 15672.28 | 0.00\% | 100.00\% |
| 175.0 | 7.080 | 0.503 | 15672.783 | 0.00\% | 100.00\% |
| 180.0 | 7.381 | 0.173 | 15672.955 | 0.00\% | 100.00\% |

## Luminous Intensity Distribution Diagram

Light Distribution Curve [Unit:cd]


C0/C180:
C90/C270:
Field angle( $10 \%$ Imax):C0/180Left:76.6 Right: 75.0
C90/270Left:74.2 Right:77.5
Beam Angle(50\%Imax):C0/180Left:55.5 Right:54.4
C90/270Left:53.5 Right:56.7

Lux distance Curve


## UGR Glare

| Illumination assessment according UGR |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rf of Ceiling | 70 | 70 | 50 | 50 | 30 | 70 | 70 | 50 | 50 | 30 |
| Rf of Wall | 50 | 30 | 50 | 30 | 30 | 50 | 30 | 50 | 30 | 30 |
| Rf of Floor | 20 | 20 | 20 | 20 | 20 | 20 | 20 | 20 | 20 | 20 |
| $\begin{array}{\|l\|} \hline \text { Room dimension } \\ \mathrm{X} \end{array}$ | Viewed crosswise |  |  |  |  | Viewed endwise |  |  |  |  |
| 2 H | 20.22 | 21.81 | 20.58 | 22.13 | 22.45 | 20.18 | 21.77 | 20.54 | 22.09 | 22.41 |
|  | 21.42 | 22.86 | 21.80 | 23.20 | 23.54 | 21.58 | 23.01 | 21.96 | 23.35 | 23.70 |
|  | 21.70 | 23.04 | 22.09 | 23.39 | 23.76 | 21.97 | 23.32 | 22.37 | 23.67 | 24.03 |
|  | 21.79 | 23.04 | 22.20 | 23.41 | 23.80 | 22.17 | 23.42 | 22.58 | 23.79 | 24.18 |
|  | 21.75 | 22.95 | 22.16 | 23.33 | 23.73 | 22.17 | 23.37 | 22.58 | 23.75 | 24.15 |
|  | 21.70 | 22.85 | 22.12 | 23.24 | 23.65 | 22.14 | 23.29 | 22.55 | 23.67 | 24.09 |
| $4 \mathrm{H} \quad 2 \mathrm{H}$ | 20.65 | 21.99 | 21.04 | 22.34 | 22.71 | 20.61 | 21.96 | 21.01 | 22.31 | 22.68 |
| 3 H | 21.98 | 23.12 | 22.40 | 23.50 | 23.92 | 22.08 | 23.22 | 22.50 | 23.60 | 24.02 |
| 4 H | 22.37 | 23.37 | 22.80 | 23.79 | 24.23 | 22.54 | 23.54 | 22.97 | 23.95 | 24.39 |
| 6 H | 22.46 | 23.35 | 22.92 | 23.79 | 24.24 | 22.72 | 23.60 | 23.18 | 24.05 | 24.49 |
| 8H | 22.46 | 23.28 | 22.93 | 23.73 | 24.19 | 22.75 | 23.58 | 23.22 | 24.02 | 24.49 |
| 12 H | 22.43 | 23.20 | 22.91 | 23.64 | 24.15 | 22.74 | 23.51 | 23.22 | 23.95 | 24.46 |
| $8 \mathrm{H} \quad 4 \mathrm{H}$ | 22.42 | 23.24 | 22.89 | 23.69 | 24.15 | 22.58 | 23.40 | 23.05 | 23.85 | 24.32 |
| 6H | 22.52 | 23.21 | 23.02 | 23.68 | 24.18 | 22.76 | 23.45 | 23.25 | 23.92 | 24.42 |
| 8H | 22.57 | 23.17 | 23.09 | 23.68 | 24.17 | 22.84 | 23.44 | 23.36 | 23.95 | 24.44 |
| 12 H | 22.55 | 23.05 | 23.07 | 23.56 | 24.07 | 22.84 | 23.34 | 23.36 | 23.85 | 24.36 |
| 12 H | 22.40 | 23.16 | 22.88 | 23.60 | 24.11 | 22.56 | 23.33 | 23.04 | 23.77 | 24.27 |
|  | 22.55 | 23.14 | 23.06 | 23.65 | 24.15 | 22.78 | 23.38 | 23.30 | 23.89 | 24.38 |
|  | 22.56 | 23.06 | 23.08 | 23.57 | 24.08 | 22.83 | 23.33 | 23.35 | 23.84 | 24.35 |
| Variation with the observer position at spacings: |  |  |  |  |  |  |  |  |  |  |
| $\mathrm{S}=1.0 \mathrm{H}$ |  | 0.4/-0.4 |  |  |  | 0.5/-0.4 |  |  |  |  |
| $\mathrm{S}=1.5 \mathrm{H}$ |  | 0.8/-0.7 |  |  |  | 0.7/-0.9 |  |  |  |  |
| $\mathrm{S}=2.0 \mathrm{H}$ |  | $1.6 /-1.7$ |  |  |  | $1.6 /-1.4$ |  |  |  |  |
| Standard tables: |  | BK2 |  |  |  | BK2 |  |  |  |  |
| Uncorrected UGR |  | 4.8 |  |  |  | $4.5$ |  |  |  |  |

UGR calculation is based on CIE Publ. $117, \mathrm{~S} / \mathrm{H}=1$

## Luminous Intensity Distribution Data

| $\mathrm{C} / \gamma\left({ }^{\circ}\right)$ | 0.0 | 5.0 | 10.0 | 15.0 | 20.0 | 25.0 | 30.0 | 35.0 | 40.0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.0 | 5891.65 | 5837.06 | 5765.17 | 5599.59 | 5423.13 | 5213.99 | 4926.41 | 4612.70 | 4274.80 |
| 22.5 | 5891.65 | 5847.95 | 5760.81 | 5588.70 | 5420.95 | 5207.45 | 4917.70 | 4617.06 | 4261.95 |
| 45.0 | 5891.65 | 5823.99 | 5743.38 | 5588.70 | 5399.17 | 5185.66 | 4917.70 | 4601.81 | 4234.72 |
| 67.5 | 5891.65 | 5806.56 | 5712.88 | 5558.20 | 5353.42 | 5137.74 | 4882.84 | 4540.81 | 4190.93 |
| 90.0 | 5891.65 | 5924.20 | 5850.13 | 5712.88 | 5534.24 | 5309.84 | 5074.56 | 4780.45 | 4436.24 |
| 112.5 | 5891.65 | 5900.24 | 5815.27 | 5667.13 | 5475.42 | 5257.56 | 5026.63 | 4721.63 | 4370.88 |
| 135.0 | 5891.65 | 5858.84 | 5765.17 | 5625.74 | 5457.99 | 5240.13 | 4976.52 | 4684.59 | 4340.38 |
| 157.5 | 5891.65 | 5841.42 | 5749.92 | 5619.20 | 5442.74 | 5220.52 | 4969.99 | 4664.99 | 4314.23 |
| 180.0 | 5891.65 | 5850.13 | 5749.92 | 5614.84 | 5449.27 | 5218.34 | 4952.56 | 4654.09 | 4298.98 |
| 202.5 | 5891.65 | 5852.31 | 5767.34 | 5625.74 | 5438.38 | 5222.70 | 4956.91 | 4651.91 | 4320.77 |
| 225.0 | 5891.65 | 5876.27 | 5771.70 | 5627.92 | 5438.38 | 5220.52 | 4974.34 | 4673.70 | 4329.48 |
| 247.5 | 5891.65 | 5863.20 | 5765.17 | 5617.02 | 5436.20 | 5224.88 | 4965.63 | 4678.06 | 4340.38 |
| 270.0 | 5891.65 | 5884.99 | 5778.24 | 5617.02 | 5429.67 | 5185.66 | 4917.70 | 4569.13 | 4196.37 |
| 292.5 | 5891.65 | 5858.84 | 5756.45 | 5590.88 | 5407.88 | 5185.66 | 4913.34 | 4588.74 | 4218.60 |
| 315.0 | 5891.65 | 5839.24 | 5754.27 | 5584.34 | 5405.70 | 5192.20 | 4919.88 | 4590.91 | 4236.02 |
| 337.5 | 5891.65 | 5850.13 | 5756.45 | 5608.31 | 5429.67 | 5207.45 | 4935.13 | 4606.16 | 4253.45 |
| 360.0 | 5891.65 | 5837.06 | 5765.17 | 5599.59 | 5423.13 | 5213.99 | 4926.41 | 4612.70 | 4274.80 |
| $\left.\mathrm{C} / \gamma^{( }{ }^{\circ}\right)$ | 45.0 | 50.0 | 55.0 | 60.0 | 65.0 | 70.0 | 75.0 | 80.0 | 85.0 |
| 0.0 | 3839.74 | 3375.49 | 2890.97 | 2341.75 | 1707.79 | 1122.62 | 589.74 | 195.20 | 2.40 |
| 22.5 | 3827.98 | 3375.49 | 2870.27 | 2320.84 | 1716.06 | 1097.57 | 577.76 | 191.06 | 2.61 |
| 45.0 | 3797.04 | 3339.32 | 2848.05 | 2293.82 | 1646.35 | 1079.05 | 542.03 | 166.66 | 2.61 |
| 67.5 | 3770.03 | 3286.38 | 2780.95 | 2257.22 | 1596.24 | 1034.61 | 502.38 | 151.85 | 2.61 |
| 90.0 | 4046.27 | 3597.48 | 3144.34 | 2612.77 | 2024.55 | 1397.12 | 835.70 | 357.94 | 51.85 |
| 112.5 | 3993.98 | 3547.38 | 3061.55 | 2545.23 | 1963.55 | 1329.59 | 802.37 | 332.23 | 13.51 |
| 135.0 | 3935.16 | 3497.27 | 3035.41 | 2506.02 | 1928.69 | 1299.09 | 761.19 | 303.04 | 3.92 |
| 157.5 | 3919.91 | 3492.91 | 3004.91 | 2492.95 | 1909.09 | 1279.48 | 745.29 | 299.55 | 4.14 |
| 180.0 | 3911.20 | 3460.23 | 2991.84 | 2484.23 | 1887.30 | 1290.37 | 732.87 | 293.02 | 4.79 |
| 202.5 | 3928.63 | 3479.84 | 3000.55 | 2477.70 | 1913.44 | 1283.84 | 744.20 | 301.52 | 4.58 |
| 225.0 | 3928.63 | 3488.55 | 3022.34 | 2510.37 | 1943.94 | 1323.05 | 774.92 | 318.73 | 5.01 |
| 247.5 | 3946.06 | 3514.70 | 3052.84 | 2547.41 | 1998.41 | 1360.09 | 816.53 | 351.19 | 16.56 |
| 270.0 | 3797.48 | 3315.79 | 2807.97 | 2248.73 | 1613.89 | 1033.30 | 512.40 | 136.82 | 2.18 |
| 292.5 | 3802.92 | 3339.98 | 2831.93 | 2295.35 | 1659.42 | 1065.32 | 542.47 | 163.39 | 2.40 |
| 315.0 | 3822.09 | 3352.61 | 2851.10 | 2313.21 | 1710.84 | 1103.01 | 570.57 | 177.12 | 2.40 |
| 337.5 | 3838.22 | 3366.12 | 2883.78 | 2339.79 | 1712.58 | 1117.83 | 591.27 | 189.75 | 2.61 |
| 360.0 | 3839.74 | 3375.49 | 2890.97 | 2341.75 | 1707.79 | 1122.62 | 589.74 | 195.20 | 2.40 |
| $\mathrm{C} / \gamma\left({ }^{\circ}\right)$ | 90.0 | 95.0 | 100.0 | 105.0 | 110.0 | 115.0 | 120.0 | 125.0 | 130.0 |
| 0.0 | 1.53 | 1.53 | 1.31 | 1.74 | 1.96 | 2.61 | 3.49 | 3.92 | 4.79 |
| 22.5 | 1.31 | 1.31 | 1.31 | 1.74 | 2.18 | 2.83 | 3.27 | 4.14 | 4.79 |
| 45.0 | 1.31 | 1.31 | 1.31 | 1.74 | 2.18 | 3.05 | 3.49 | 4.14 | 5.01 |
| 67.5 | 1.53 | 1.09 | 1.53 | 1.74 | 2.18 | 2.83 | 3.49 | 4.36 | 5.23 |
| 90.0 | 1.53 | 1.09 | 0.87 | 1.31 | 1.53 | 2.18 | 2.83 | 3.70 | 4.58 |
| 112.5 | 1.31 | 1.09 | 0.87 | 1.31 | 1.74 | 2.61 | 2.83 | 3.92 | 4.36 |
| 135.0 | 1.31 | 0.87 | 0.87 | 1.31 | 1.74 | 2.40 | 3.05 | 3.92 | 4.58 |
| 157.5 | 1.09 | 1.09 | 1.09 | 1.31 | 1.74 | 2.40 | 3.05 | 3.70 | 4.58 |
| 180.0 | 1.31 | 1.09 | 0.87 | 1.53 | 1.74 | 2.40 | 3.05 | 3.70 | 4.36 |
| 202.5 | 1.09 | 0.87 | 0.87 | 1.53 | 1.74 | 2.40 | 3.05 | 3.92 | 4.58 |
| 225.0 | 1.31 | 1.09 | 1.09 | 1.31 | 1.53 | 2.61 | 3.05 | 3.92 | 4.36 |
| 247.5 | 1.31 | 1.09 | 0.87 | 1.53 | 1.74 | 2.40 | 3.27 | 3.92 | 4.58 |
| 270.0 | 0.87 | 1.09 | 1.53 | 1.74 | 1.96 | 2.61 | 3.70 | 4.36 | 5.01 |
| 292.5 | 1.31 | 1.31 | 1.09 | 1.74 | 1.96 | 2.83 | 3.49 | 4.36 | 5.01 |
| 315.0 | 1.31 | 1.09 | 1.31 | 1.31 | 1.96 | 2.83 | 3.27 | 4.14 | 4.58 |
| 337.5 | 1.53 | 1.31 | 1.53 | 1.53 | 2.40 | 2.61 | 3.49 | 4.14 | 4.58 |
| 360.0 | 1.53 | 1.53 | 1.31 | 1.74 | 1.96 | 2.61 | 3.49 | 3.92 | 4.79 |


| $\mathrm{C} / \gamma\left({ }^{\circ}\right)$ | 135.0 | 140.0 | 145.0 | 150.0 | 155.0 | 160.0 | 165.0 | 170.0 | 175.0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.0 | 5.45 | 5.66 | 6.10 | 6.54 | 6.97 | 6.97 | 7.19 | 6.97 | 7.41 |
| 22.5 | 5.23 | 5.88 | 6.10 | 6.75 | 6.97 | 6.97 | 6.97 | 6.97 | 7.19 |
| 45.0 | 5.45 | 5.88 | 6.32 | 6.75 | 7.19 | 7.41 | 7.19 | 6.97 | 7.63 |
| 67.5 | 5.88 | 6.10 | 6.54 | 6.97 | 7.19 | 7.19 | 7.19 | 7.19 | 7.41 |
| 90.0 | 5.23 | 5.66 | 5.88 | 6.54 | 6.75 | 6.97 | 6.75 | 6.97 | 6.75 |
| 112.5 | 5.23 | 5.88 | 6.32 | 6.54 | 6.75 | 7.19 | 6.97 | 6.97 | 6.75 |
| 135.0 | 5.01 | 5.66 | 6.10 | 6.54 | 6.97 | 6.97 | 6.97 | 6.97 | 6.75 |
| 157.5 | 5.01 | 5.66 | 5.88 | 6.32 | 6.75 | 6.97 | 6.75 | 6.54 | 6.97 |
| 180.0 | 4.79 | 5.66 | 6.10 | 6.54 | 6.97 | 6.97 | 6.97 | 6.75 | 6.75 |
| 202.5 | 5.45 | 5.45 | 5.88 | 6.54 | 6.75 | 6.97 | 6.75 | 6.75 | 6.75 |
| 225.0 | 5.45 | 5.45 | 6.32 | 6.54 | 6.97 | 7.19 | 6.97 | 6.97 | 6.97 |
| 247.5 | 5.23 | 5.88 | 6.32 | 6.54 | 7.19 | 6.97 | 6.97 | 7.19 | 6.75 |
| 270.0 | 5.66 | 6.10 | 6.75 | 7.19 | 7.19 | 7.19 | 6.97 | 7.19 | 7.41 |
| 292.5 | 5.45 | 5.88 | 6.54 | 6.97 | 6.97 | 7.19 | 7.41 | 6.97 | 7.41 |
| 315.0 | 5.45 | 6.10 | 6.32 | 6.75 | 6.97 | 6.97 | 6.97 | 7.19 | 7.19 |
| 337.5 | 5.23 | 5.88 | 6.10 | 6.54 | 6.75 | 6.75 | 6.97 | 6.97 | 7.19 |
| 360.0 | 5.45 | 5.66 | 6.10 | 6.54 | 6.97 | 6.97 | 7.19 | 6.97 | 7.41 |


| $\mathrm{C} / \gamma\left({ }^{\circ}\right)$ | 180.0 |
| :--- | :--- |
| 0.0 | 7.38 |
| 22.5 | 7.38 |
| $\mathbf{4 5 . 0}$ | 7.38 |
| 67.5 | 7.38 |
| 90.0 | 7.38 |
| 112.5 | 7.38 |
| 135.0 | 7.38 |
| 157.5 | 7.38 |
| 180.0 | 7.38 |
| 202.5 | 7.38 |
| 225.0 | 7.38 |
| 247.5 | 7.38 |
| 270.0 | 7.38 |
| 292.5 | 7.38 |
| 315.0 | 7.38 |
| 337.5 | 7.38 |
| 360.0 | 7.38 |

## 4 Additional Test

## Electrical data at 277V

| Model Number | Test Voltage (V) | Frequency(Hz) | Power Factor | THD |
| :---: | :---: | :---: | :---: | :---: |
| CHB3-100-D-MV-30K-170S | 277 | 60 | 0.951 | $7.1 \%$ |
| CHB3-100-D-MV-65K-170S | 277 | 60 | 0.964 | $5.9 \%$ |

## 5 Performance Assessment

| Model name | CCT(K) | Total Luminous(lm) | Power(W) | Luminous Efficacy $(\mathrm{lm} / \mathrm{W})$ |
| :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { CHB3-100-D-MV- } \\ 30 \mathrm{~K}-170 \mathrm{~S} \end{gathered}$ | 3000 | 15685.24 | 99.78 | 157.2 |
| $\begin{gathered} \text { CHB3-100-D-MV- } \\ 35 \mathrm{~K}-170 \mathrm{~S} \end{gathered}$ | 3500 | $15959.62^{* 1}$ | $99.90^{*}$ | 159.8 *3 |
| $\begin{gathered} \text { CHB3-100-D-MV- } \\ 40 \mathrm{~K}-170 \mathrm{~S} \end{gathered}$ | 4000 | $16234.01^{* 1}$ | $99.90^{*}$ | 162.5 *3 |
| $\begin{gathered} \text { CHB3-100-D-MV- } \\ 45 \mathrm{~K}-170 \mathrm{~S} \end{gathered}$ | 4500 | $16508.39{ }^{* 1}$ | $99.90^{*}$ | 165.3 *3 |
| $\begin{gathered} \text { CHB3-100-D-MV- } \\ 50 \mathrm{~K}-170 \mathrm{~S} \end{gathered}$ | 5000 | $16782.77{ }^{* 1}$ | $99.90^{*}$ | 168.0 *3 |
| $\begin{gathered} \text { CHB3-100-D-MV- } \\ 57 \mathrm{~K}-170 \mathrm{~S} \end{gathered}$ | 5700 | $17057.16^{* 1}$ | 99.90*2 | $170.8{ }^{* 3}$ |
| $\begin{gathered} \text { CHB3-100-D-MV- } \\ 65 \mathrm{~K}-170 \mathrm{~S} \end{gathered}$ | 6500 | 17331.54 | 100.01 | 173.3 |

${ }^{*}$ 1: This value is calculated and the calculation formula is as below:
$15959.62=(17331.54-15685.24) / 6+15685.24$
$16234.01=(17331.54-15685.24) / 6+15959.62$
$16508.39=(17331.54-15685.24) / 6+16234.01$
16782.77=(17331.54-15685.24)/6+16508.39
17057.16=(17331.54-15685.24)/6+16782.77
*2: This value is calculated and the calculation formula is as below:
$99.90=(99.78+100.01) / 2$
*3: This value is calculated and the calcuation formula is as below:
$159.8=15959.62 / 8.04$
$162.5=16234.01 / 8.04$
$165.3=16508.39 / 8.04$
$168.0=16782.77 / 8.04$
$170.8=17057.16 / 8.04$

## Photo Document


****End of test report****


[^0]:    Jolors are for visual orientation purposes only. Created with the ANSI/IES TM-30-18 Calculator Version 2.00 .

